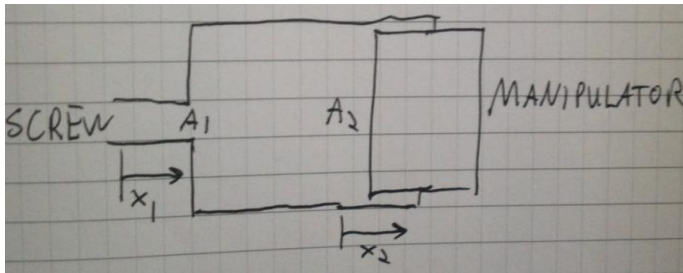
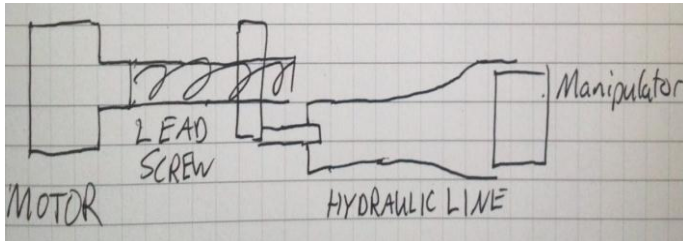


Feasibility Analysis: Resolution Considerations



- Configuration of the following yields sub 100 NM resolution
 - 1) Motor capable of 1.8 degree resolution
 - 2) Lead Screw with 0.635 mm lead
 - 3) Hydraulic area ratio of 1:64, or 80 mm inch to 8 mm diameters ratios

- Motivation: Determine Resolution of entire system. Develop relation between Motor θ and output X

From conservation of mass:

$$X_1 A_1 = X_2 A_2$$

$$X_2 = \frac{A_1}{A_2} X_1$$

- Lead Screw

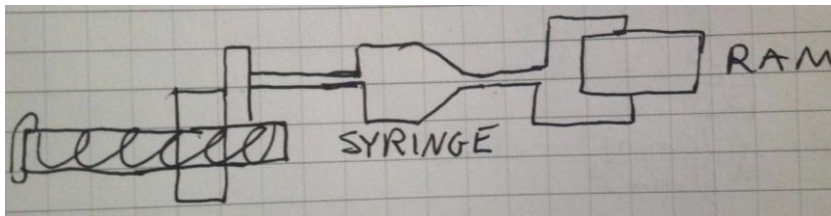
- 1 turn X_1 moves the screw lead
- Therefore, $X_2 = \frac{A_1}{A_2} l$
- Manipulator Position = $\frac{A_1}{A_2} l * \#turns$

$$X_2 = \frac{A_1}{A_2} l * \frac{\#degrees}{360}$$

$$100e-9 = \frac{A_1}{A_2} .635 \left(\frac{1.8}{360} \right) \longrightarrow .0314 = \frac{A_1}{A_2}$$

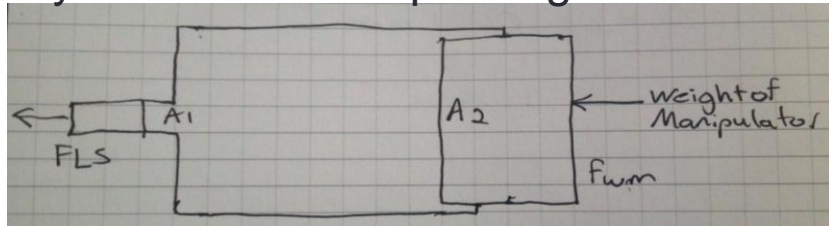
Feasibility Analysis: Motor torque Requirements

Motivation: Estimate Motor torque to pump system.



Worst case loading is actuation of stage in vertical axis.

Hydraulic force req = weight of device



Internal pressures equal. Therefore,

$$f_{LS} * A1 = f_{wm} * A2$$

$$f_{LS} = \frac{A1}{A2} f_{wm}$$

Lead Screw Torque Estimation

F = force req = fls

$$T_{LS} = \frac{F_{dm}}{2} \left(\frac{L + \pi \mu d m}{\pi d m - \mu L} \right)$$

dm = mean diameter = 6.35mm

μ = coef of friction = .25

L = lead = .635 mm/rotation

Area ratio 64:1

Force estimated at 9.8 N

$$T_{LS} = \frac{64}{1} * \frac{1 * 9.81 * .25}{2} * \frac{.635 + \pi * 6.35 * .25}{\pi * 6.35 - 6.35 * .635} = 0.508 \text{ N} * \text{m} = 72 \text{ in} * \text{oz}$$

Typical motor produces 25 to 200 in*oz

- Conservative estimates a require motor torque of no more then 72 in*oz
- This is well with in the usual operating range of normal motors